



# *High Resolution Computational Unsteady Aerodynamic Techniques Applied to Maneuvering Unmanned Combat Aircraft*

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# Outline



## ♦ Overview and motivation

- UCAV Simulation Issues
- Simulation hierarchies

## ♦ Static Case Validation of DES

## ♦ Forced Motion Validation of DES

## ♦ Embedded LES Modifications to DES

## ♦ Future Areas of Research Necessary

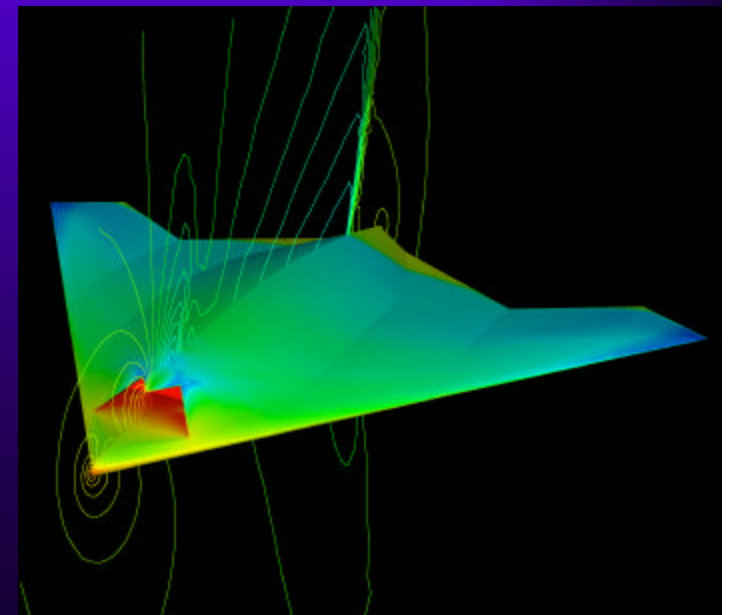
## ♦ Conclusions



# UCAV Simulation Issues

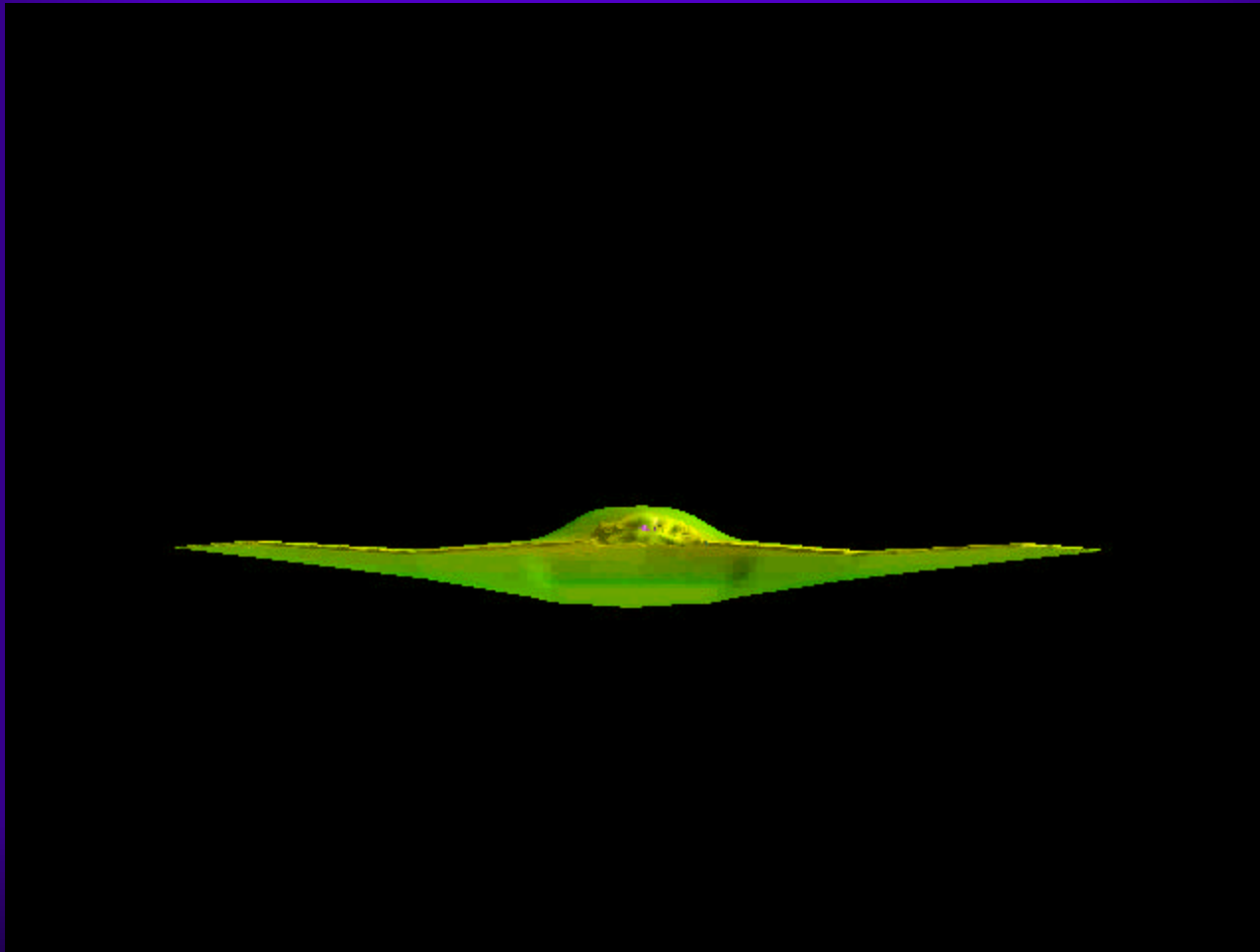


- Unmanned Combat Air Vehicles are capable of super-maneuverability
- Main Challenges
  - Maneuvers occur at **high Reynolds numbers** for which the underlying fluid motion is usually **turbulent**
  - Incorporates massively separated flows and complicated vortical flows
  - Complete simulation requires solid-body motion, 6-DOF, and aeroelasticity
- Wind tunnel tests problematic
  - Important Reynolds number effects
  - Motion mechanical systems intrusive
- Flight tests costly, time-consuming
- Computational modeling an important element for advancing fundamental understanding and engineering prediction





# Unmanned Combat Air Vehicles (UCAV)



Simulation provided by Mr Ken Wurtzler, Cobalt Solutions LLC



# Massive Separations/Vortical Flowfields



## ♦ Challenges and issues

- flow fields are inherently unsteady, chaotic, and three-dimensional
  - » accuracy is crucial at high angle of attack: lift, drag, and moments
  - » complex nature of massive separation/vortical flowfields
    - defeats conventional turbulence models
    - higher fidelity computational techniques required
- flow fields are described by the Navier-Stokes equations
  - » analytical solution for aircraft not possible

# Choice of the computational model

## ♦ Direct Numerical Simulation (DNS)

- solution of the Navier-Stokes equations without use of an explicit turbulence – limited to low Reynolds numbers
- powerful research tool
- *ready for full aircraft in ~2080*

## ♦ Large Eddy Simulation (LES)

- direct resolution of the large, energy-containing scales of the turbulent flow, model only the small eddies
- high computational cost in boundary layers
- *ready for full aircraft in ~2045*

## ♦ Reynolds-average Navier-Stokes (RANS)

- model the entire spectrum of turbulent motions
- Highly unreliable performance in separated flows
- *ready for full aircraft today*

increase in cost



increase in empiricism

DES method combines RANS and LES



# Detached-Eddy Simulation (DES)



- ◆ Turbulence modeling approach proposed by Spalart *et al.* (1997)
  - Combines **Large Eddy Simulation**, and **Reynolds-Averaged** approaches
  - Designed to provide **accurate solutions for massively separated flows**
  - Can resolve **unsteady flow features**
    - » Aero-acoustics, aero-elasticity
  - RANS model responsible for **predicting BL growth and separation (NUMERICALLY FEASIBLE)**
  - LES model responsible for **prediction of unsteady flow in separated region (ACCURATE)**





# Flow Solver – Cobalt



- ♦ **CHSSI Developed**
- ♦ **Hybrid-Unstructured, Compressible Solver**
- ♦ **Spatial Operator**
  - Riemann Solver
  - Least Squares Gradients
  - TVD limiting
  - Second order accurate
- ♦ **Temporal integration**
  - Point-implicit
  - Newton sub-iteration
  - Second order accurate
- ♦ **Parallel Performance**
  - Domain decomposition using ParMETIS
  - MPI
  - Over 98% efficient on 1024 processors



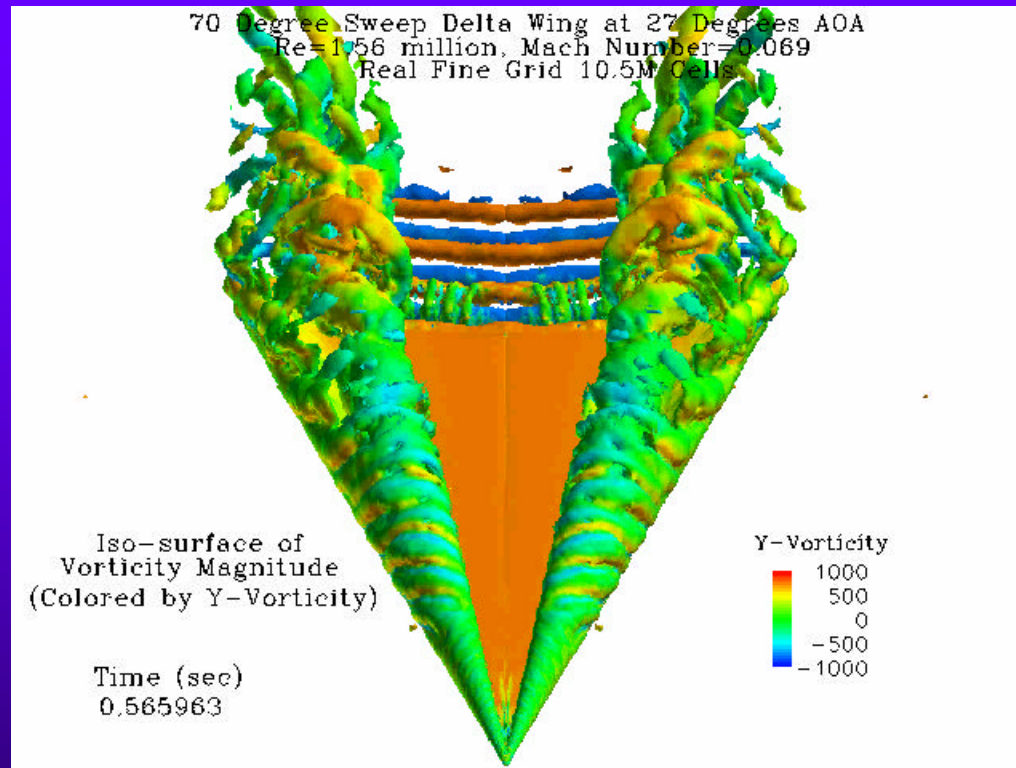
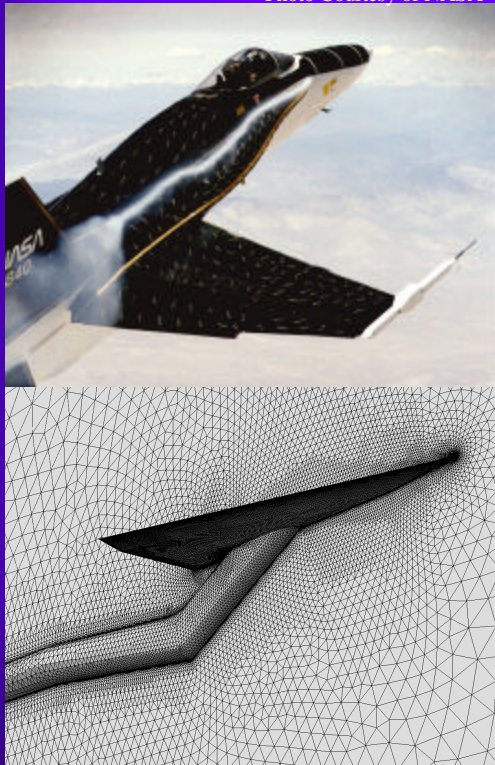
# Static Case Validation of Detached Eddy Simulation



# Delta Wing Vortex Breakdown



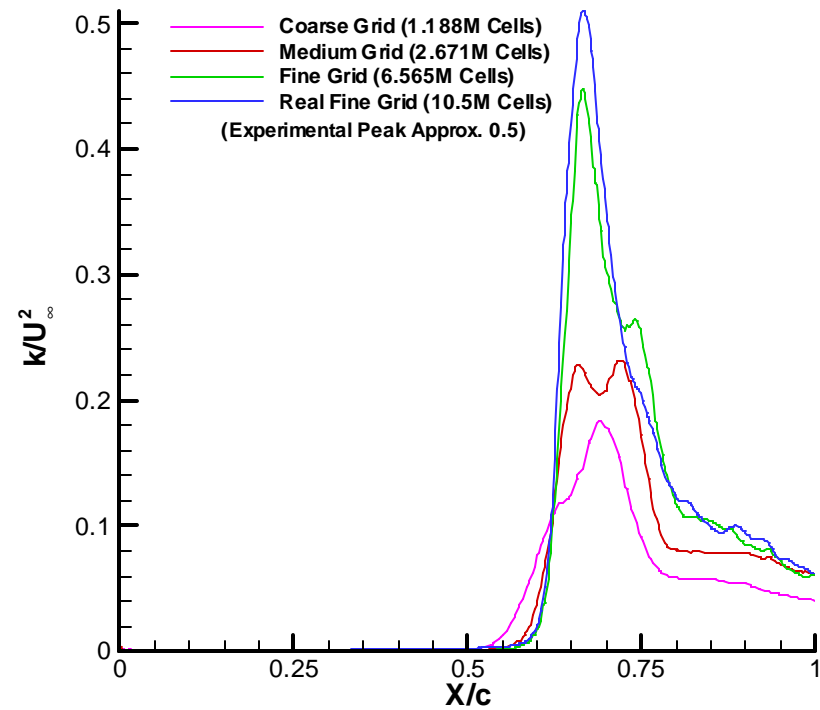
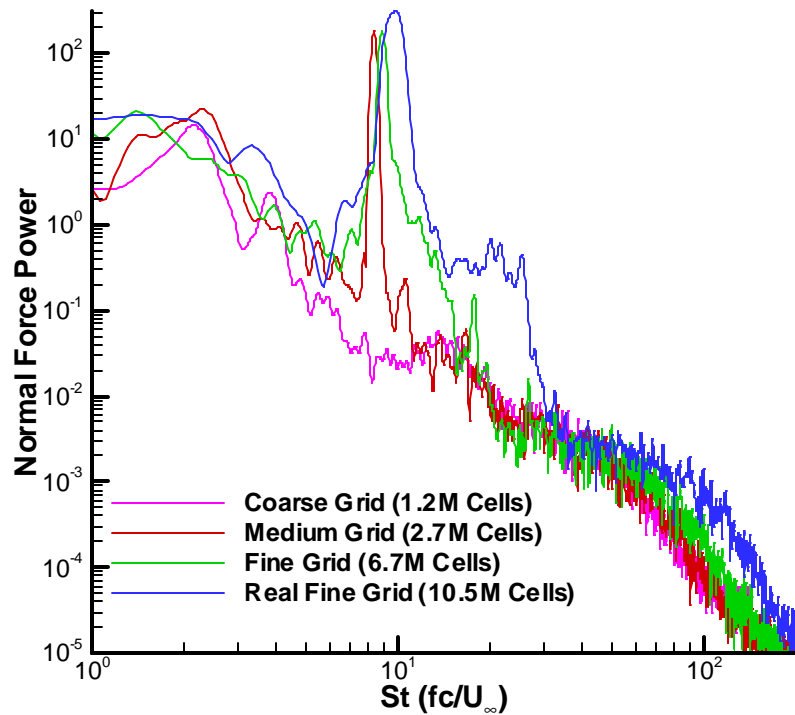
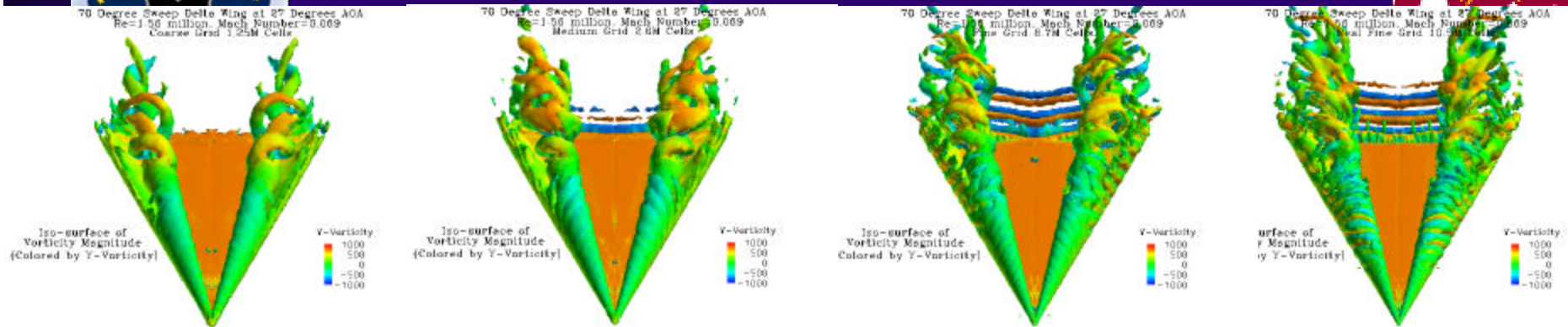
Photo Courtesy of NASA



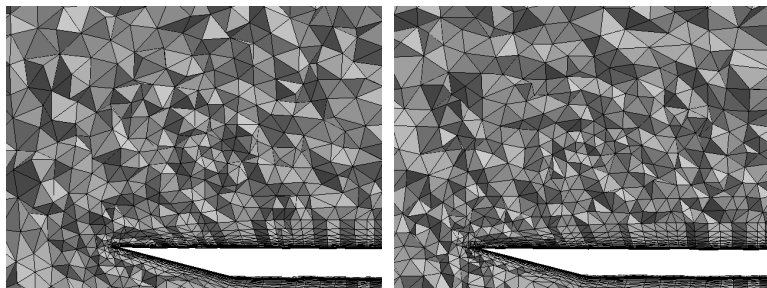
- ❖ Scott Morton (PI), Jim Forsythe, Tony Mitchell
- ❖ AFOSR project: Aeroelasticity predictions  
(PM: Tom Beutner, John Schmisser)
- ❖ AIAA 02-0587



# Grid Sensitivity Study

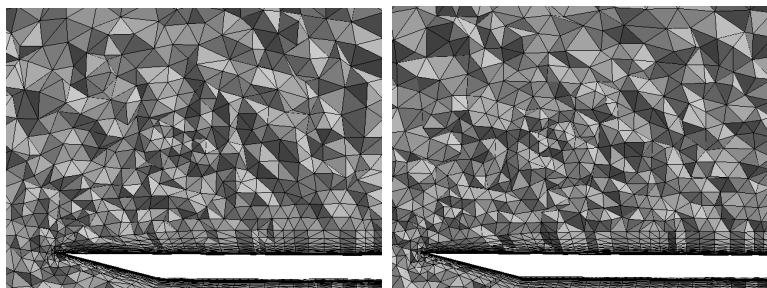


Coarse Grid



X=500 mm

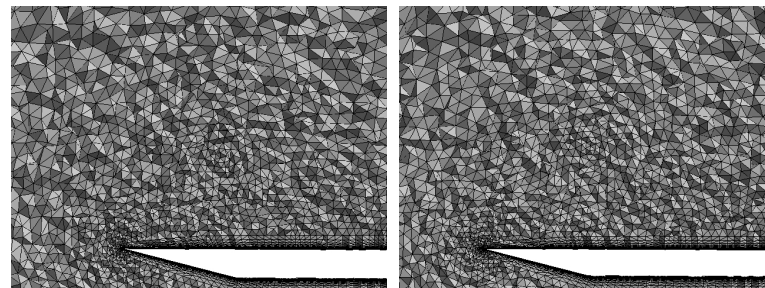
X=600mm



X=700mm

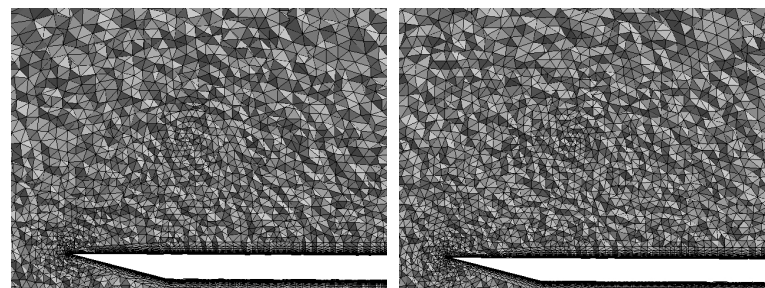
X=800mm

Real Fine Grid



X=500 mm

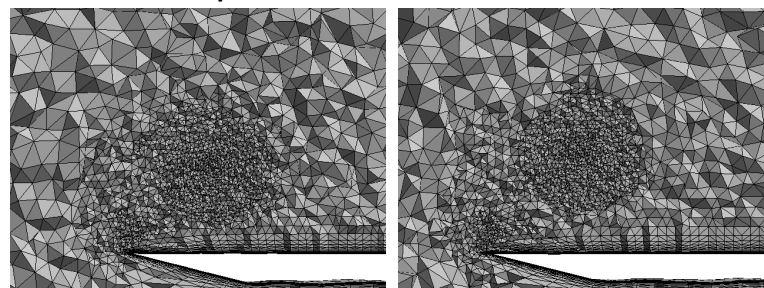
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X=700mm

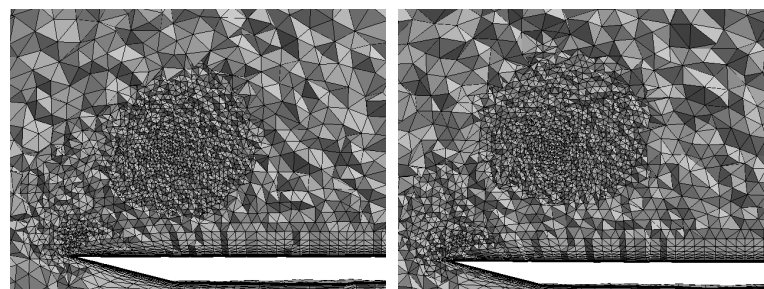
X=800mm

Adaptive Mesh Refinement Grid



X=500 mm

X=600mm



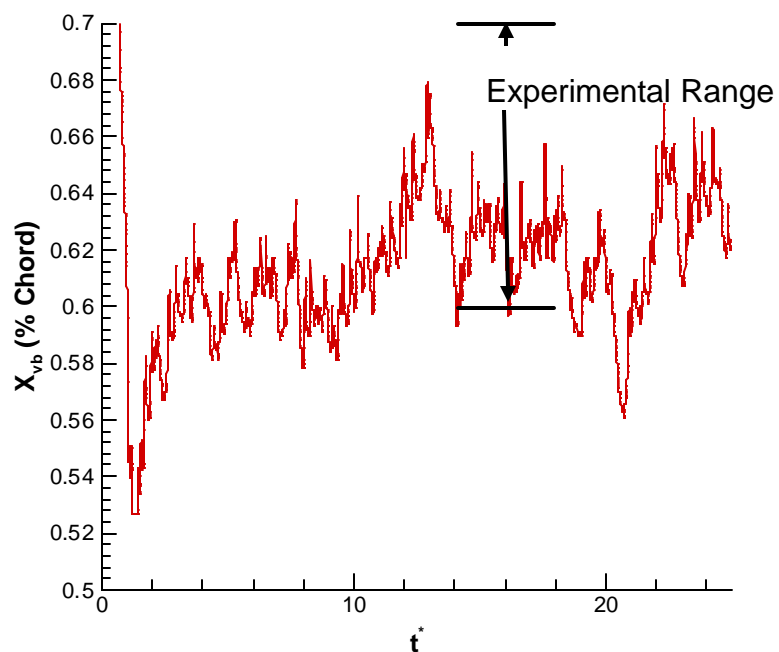
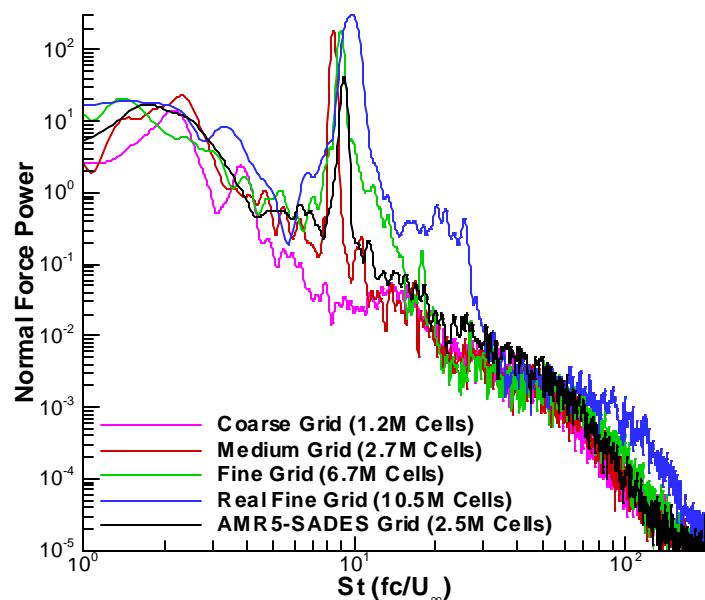
X=700mm

X=800mm

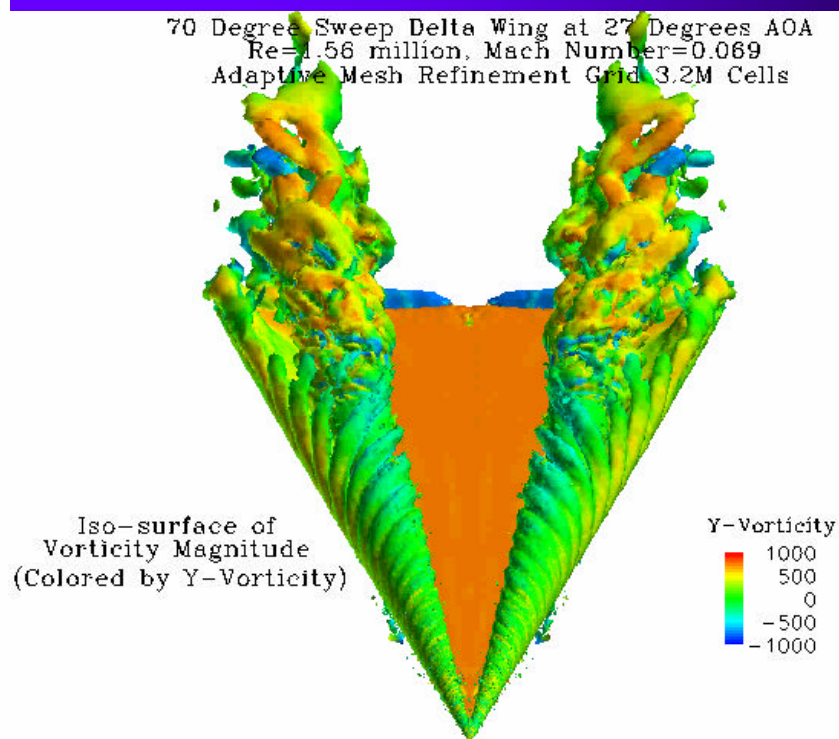




# Normal Force Power Spectral Density Analysis

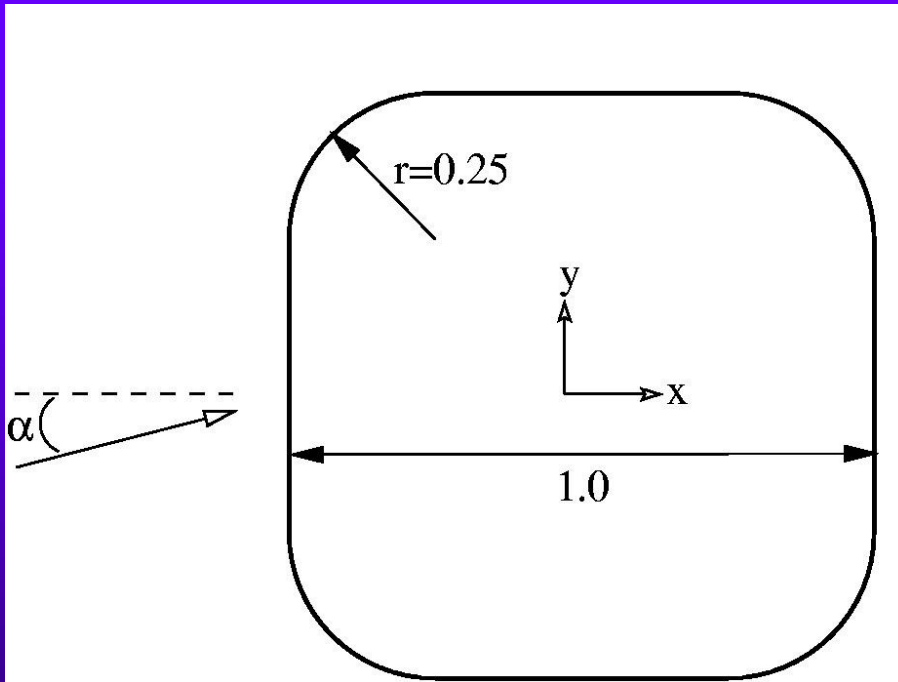


70 Degree Sweep Delta Wing at 27 Degrees AOA  
Re=1.56 million, Mach Number=0.069  
Adaptive Mesh Refinement Grid 3.2M Cells





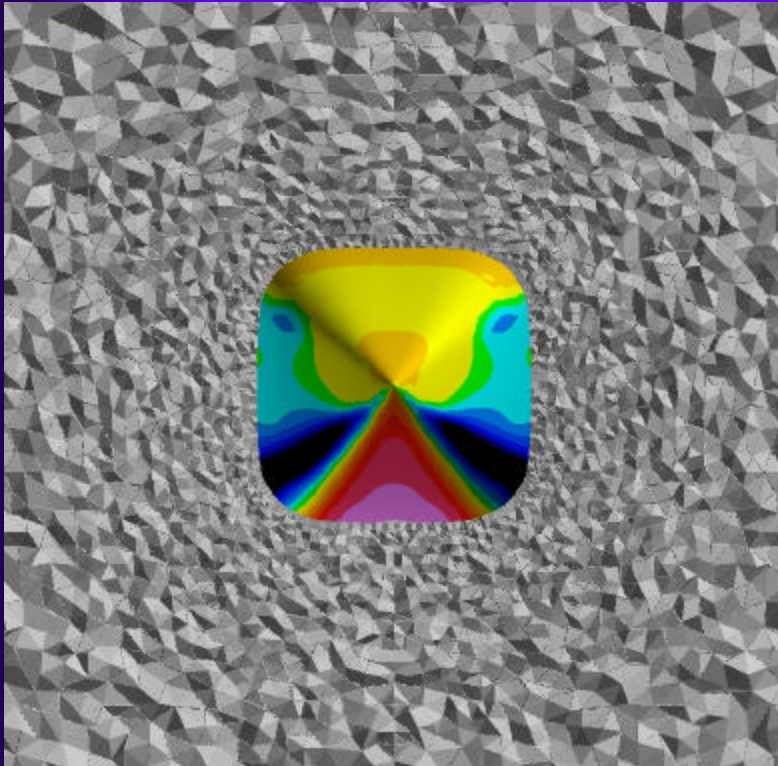
## 2D Square with Rounded Corners



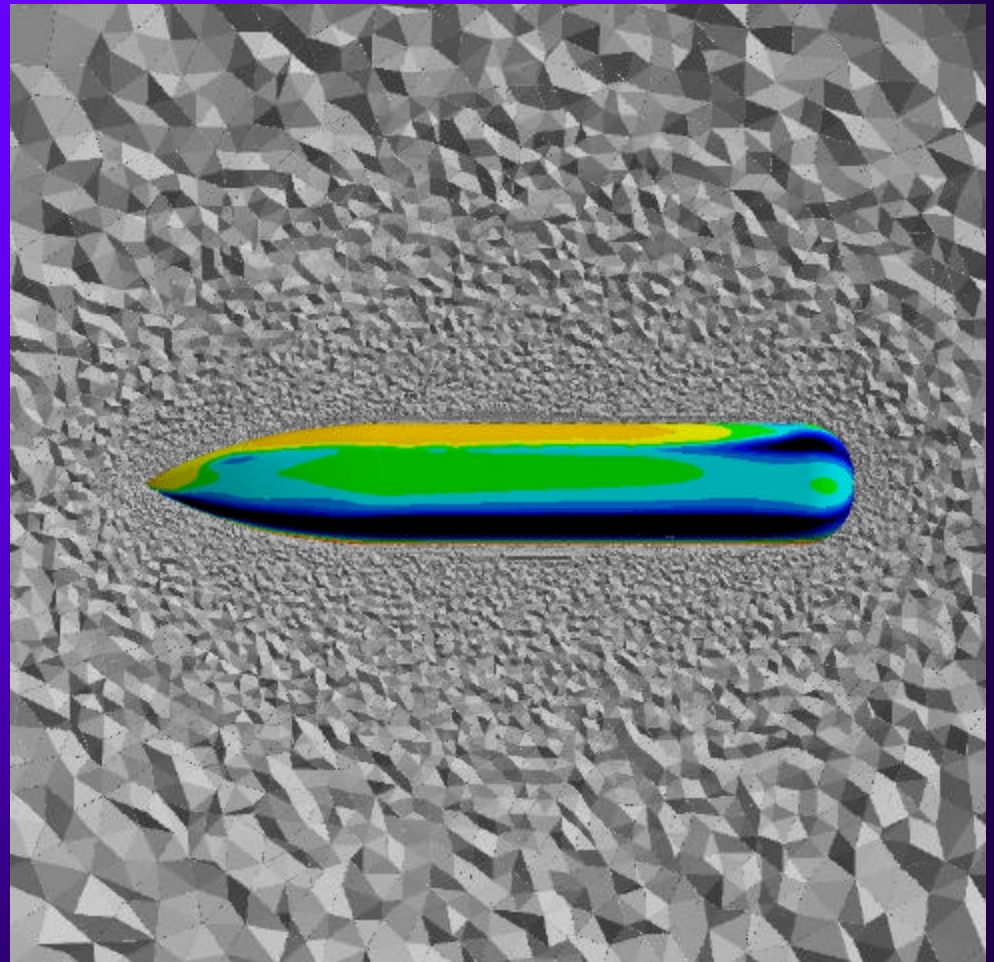
- ♦ Data of Polhamus
- ♦  $Re=800,000$
- ♦  $\alpha=10^\circ$
- ♦ Computations made on structured and unstructured grids of various domain sizes and grid spacing

- ❖ Kyle Squires (PI), Jim Forsythe, Philippe Spalart
- ❖ AFOSR project: Spin prediction (PM: Tom Beutner)
- ❖ DNS/LES IV, ERCOFTAC Vol 8

# Rectangular Ogive - 90°



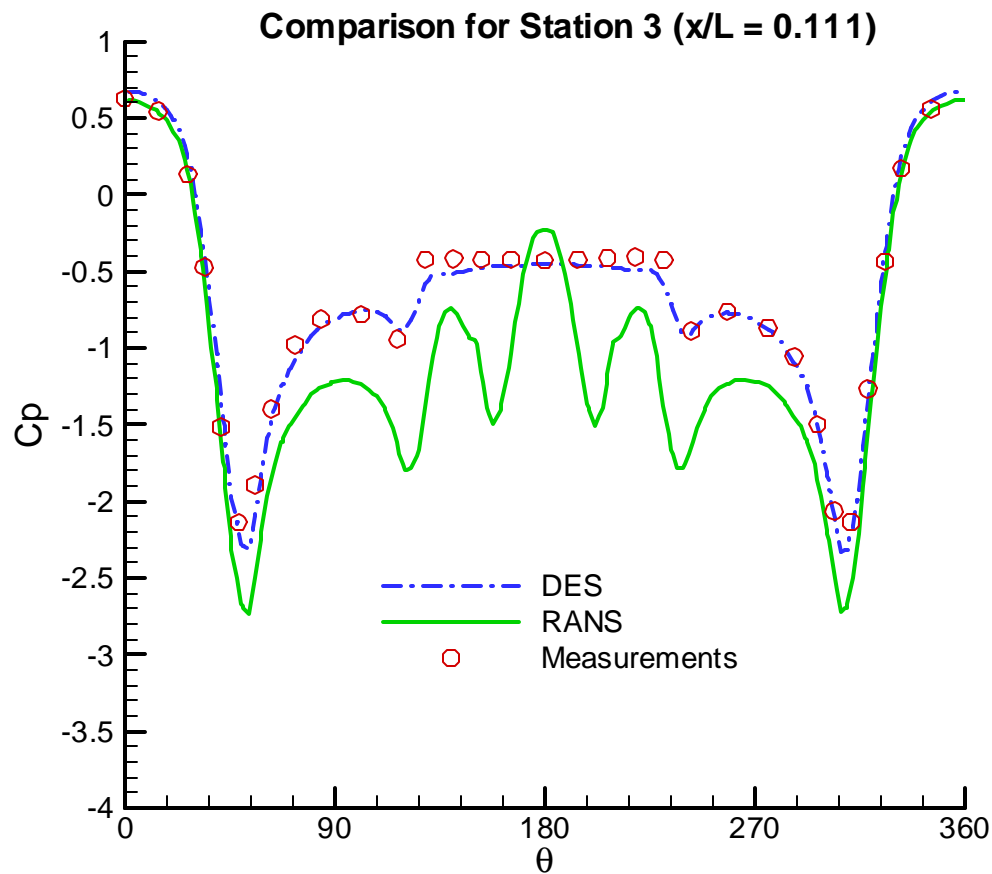
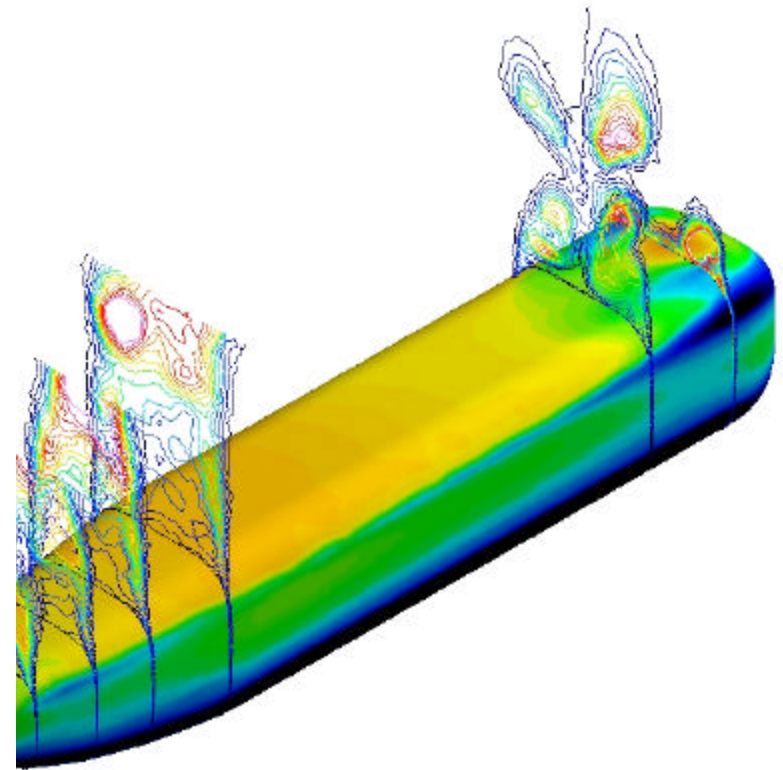
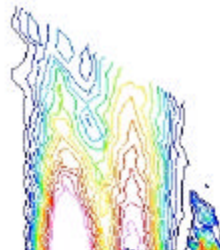
*rounded-square cross section  
corner radius is 1/4 of the  
diameter*



*6:1 rectangular ogive  
main section 3.5b  
endcap 0.5b*



# Planar Cuts of Eddy Viscosity



*DES*

pressure

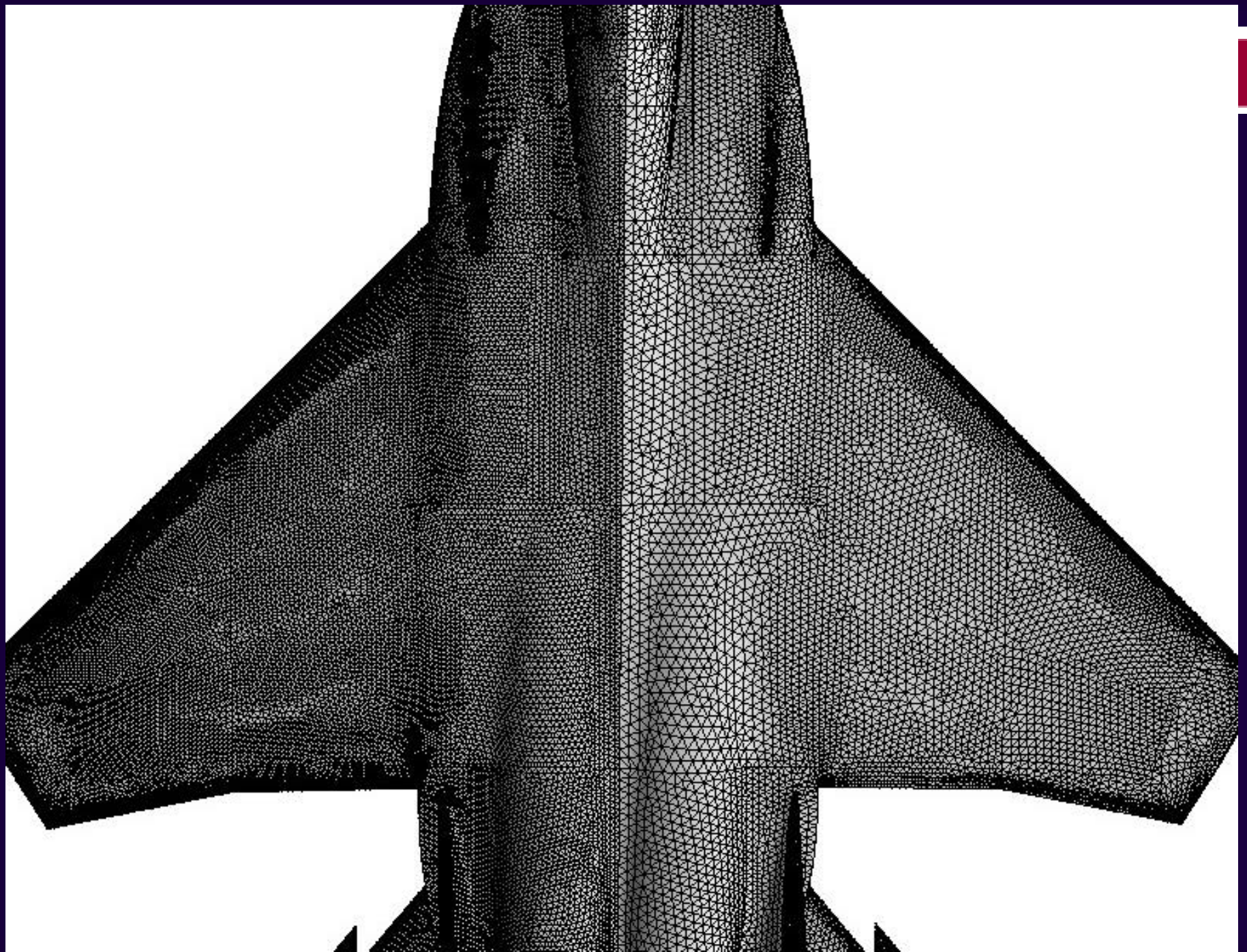


## F-15E at 65° alpha



- ♦ **Grid consists of 5.9M cells (half aircraft)**
  - Prisms in the boundary layer (using blacksmith)
    - » Conversions to prisms saved 2M cells
  - Tetrahedrons elsewhere
  - Average first  $y^+=0.7$
  - One man-week to create
  - $Re=13.6 \times 10^6$
- ♦ **2 days to compute 10,000 iterations on 256 processors (*tempest* - MHPCC)**
- ♦ **Time step and grid sensitivity examined**

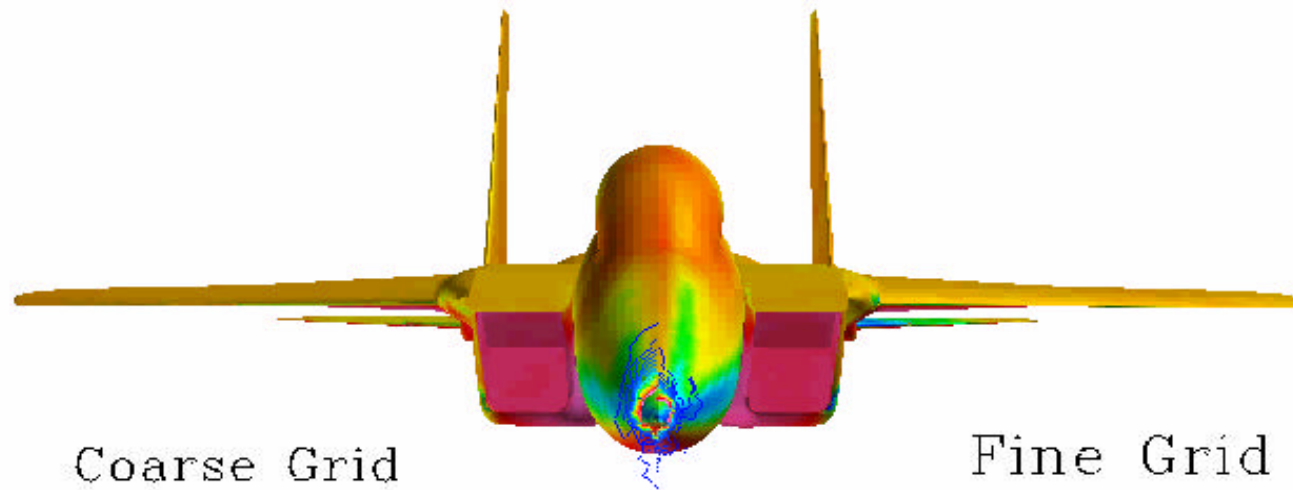
- ❖ **Jim Forsythe (PI), Kyle Squires, Ken Wurtzler, Philippe Spalart**
- ❖ **AFOSR project: Spin prediction (PM: Tom Beutner)**
- ❖ **AIAA 02-0591**

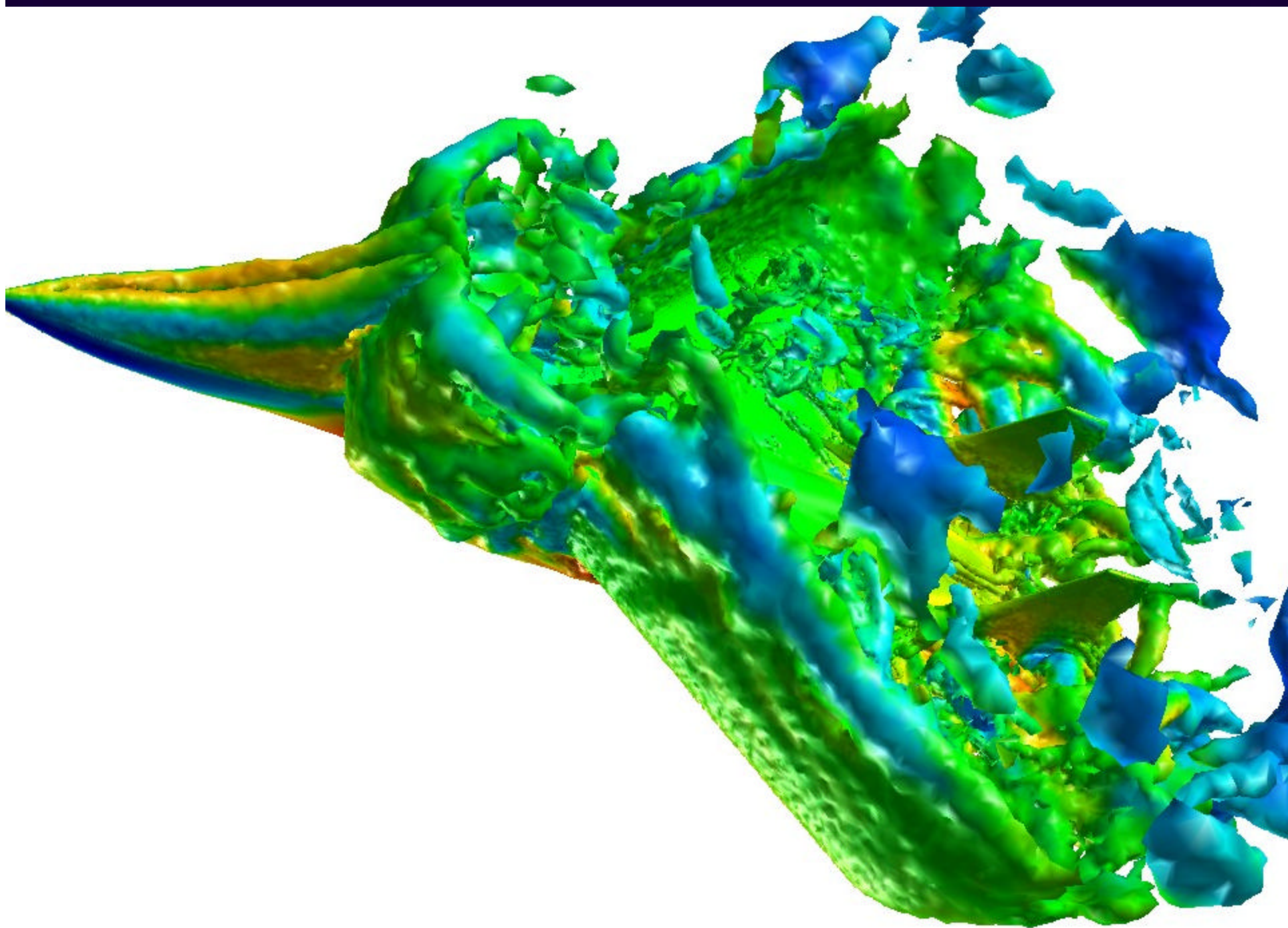






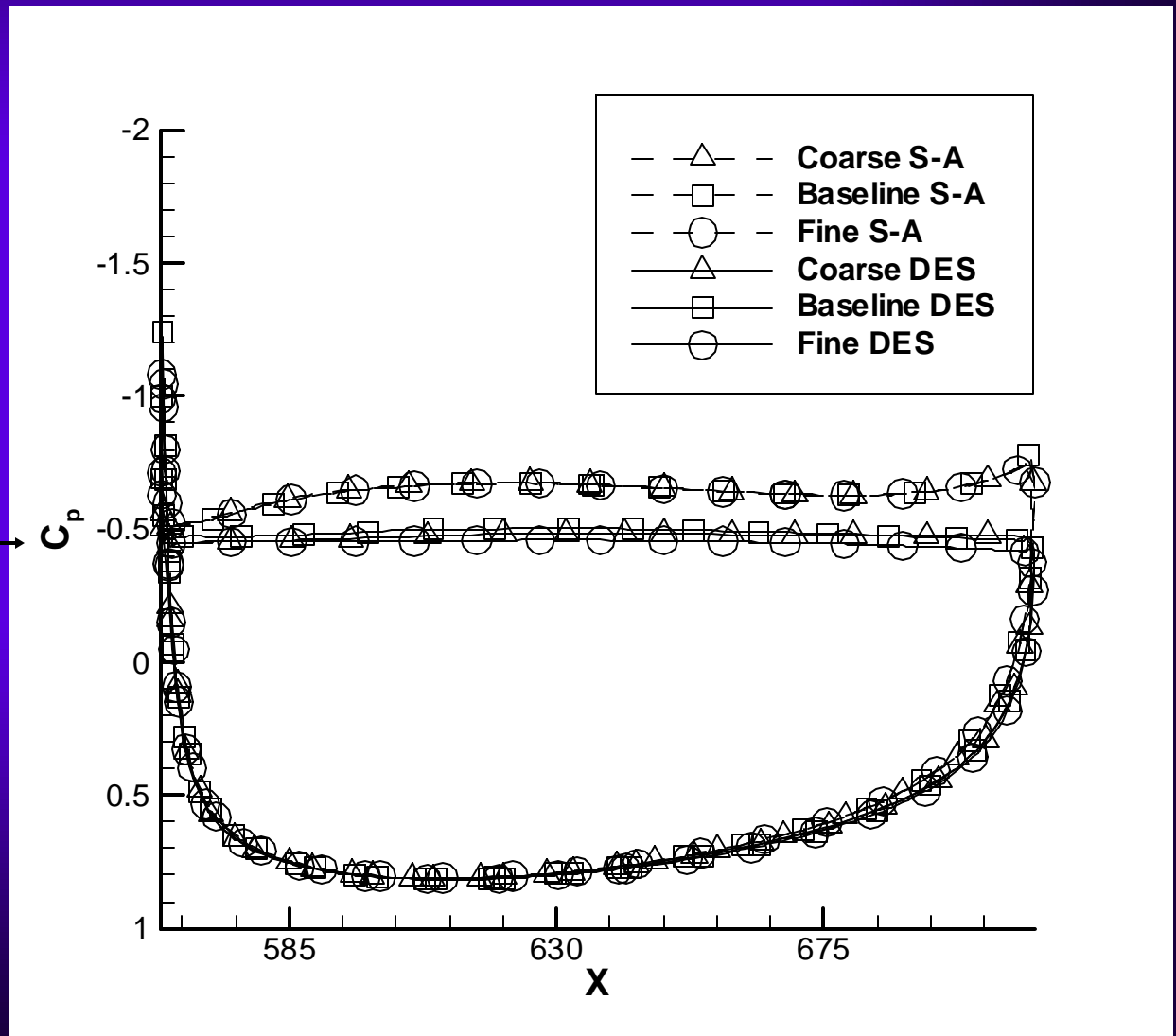
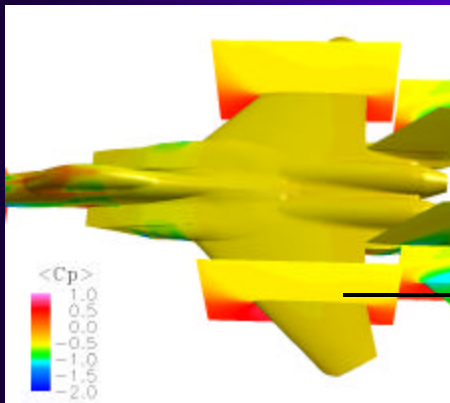
# Grid Refinement







# Time Averaged Pressures





# Integrated Forces

		$C_L$	$C_D$	$C_M$	$\%C_L$	$\%C_D$	$\%C_M$
	Exp	0.781	1.744	-0.466			
	Coarse	0.747	1.677	-0.431	-4.25%	3.86%	-7.62%
DES	Baseline	0.736	1.616	-0.495	-5.70%	-7.35%	6.10%
	Fine	0.759	1.648	-0.457	-2.81%	-5.52%	-2.00%
	Coarse	0.855	1.879	-0.504	9.49%	7.73%	8.17%
S-A	Baseline	0.852	1.867	-0.523	9.09%	7.05%	12.22%
	Fine	0.860	1.880	-0.507	10.22%	7.78%	8.72%

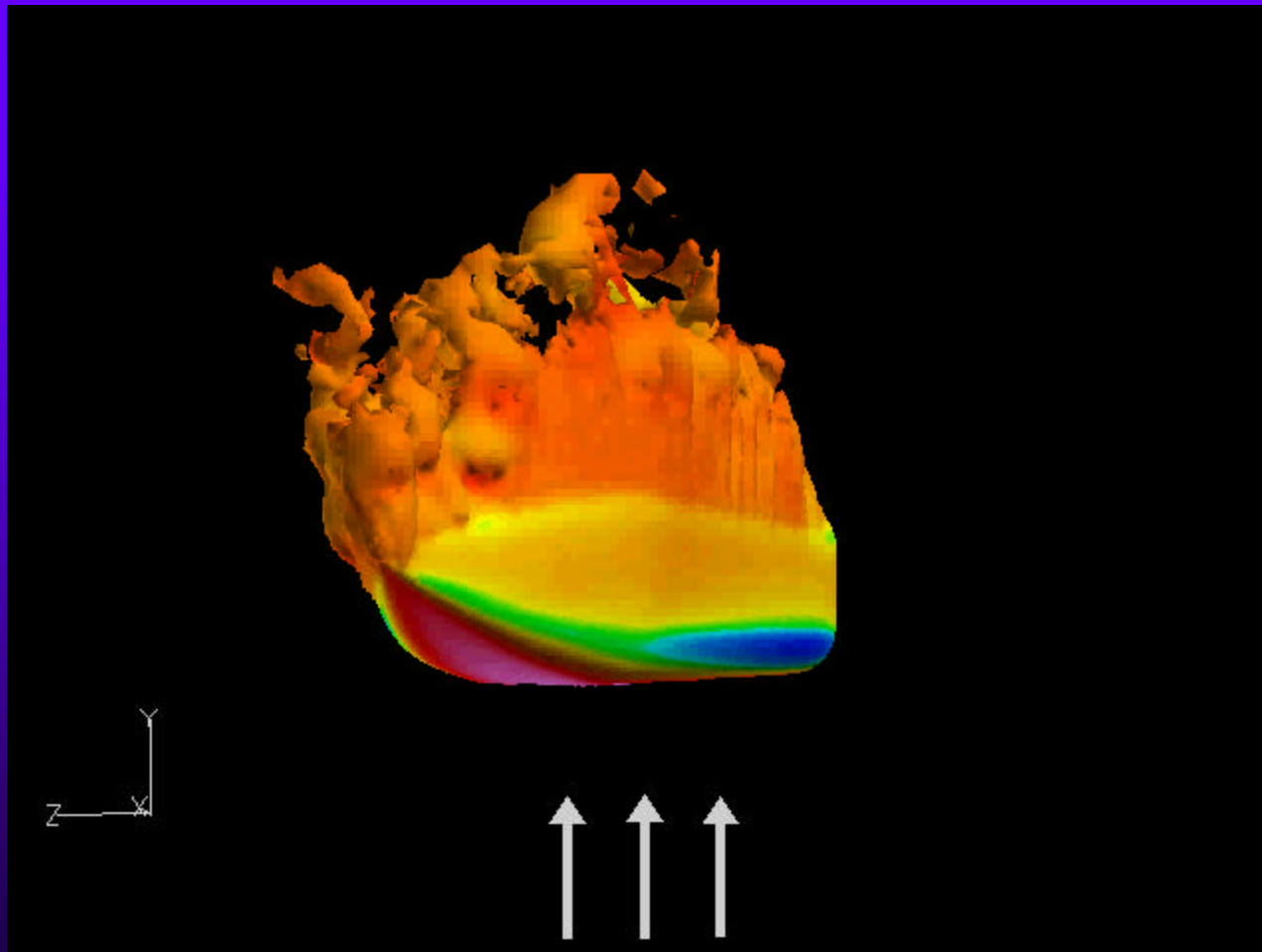


# Forced Motion Validation of Detached Eddy Simulation



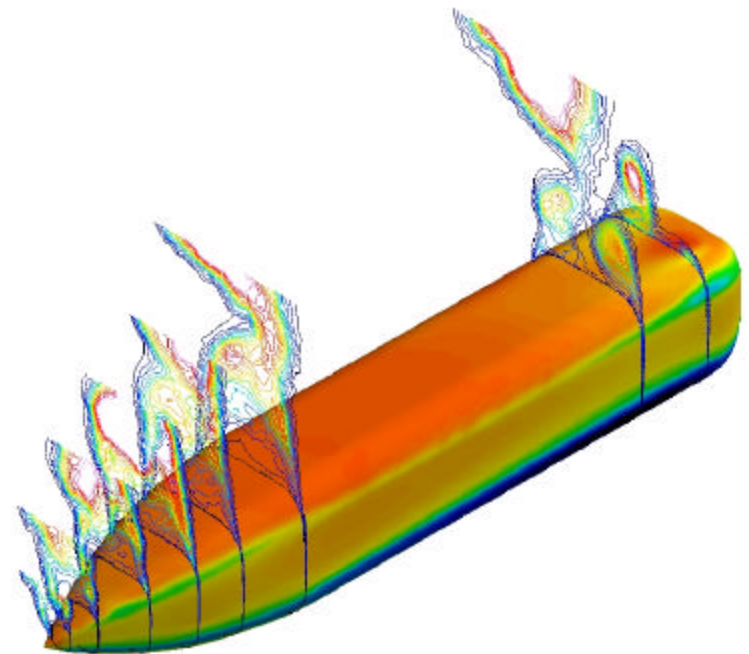
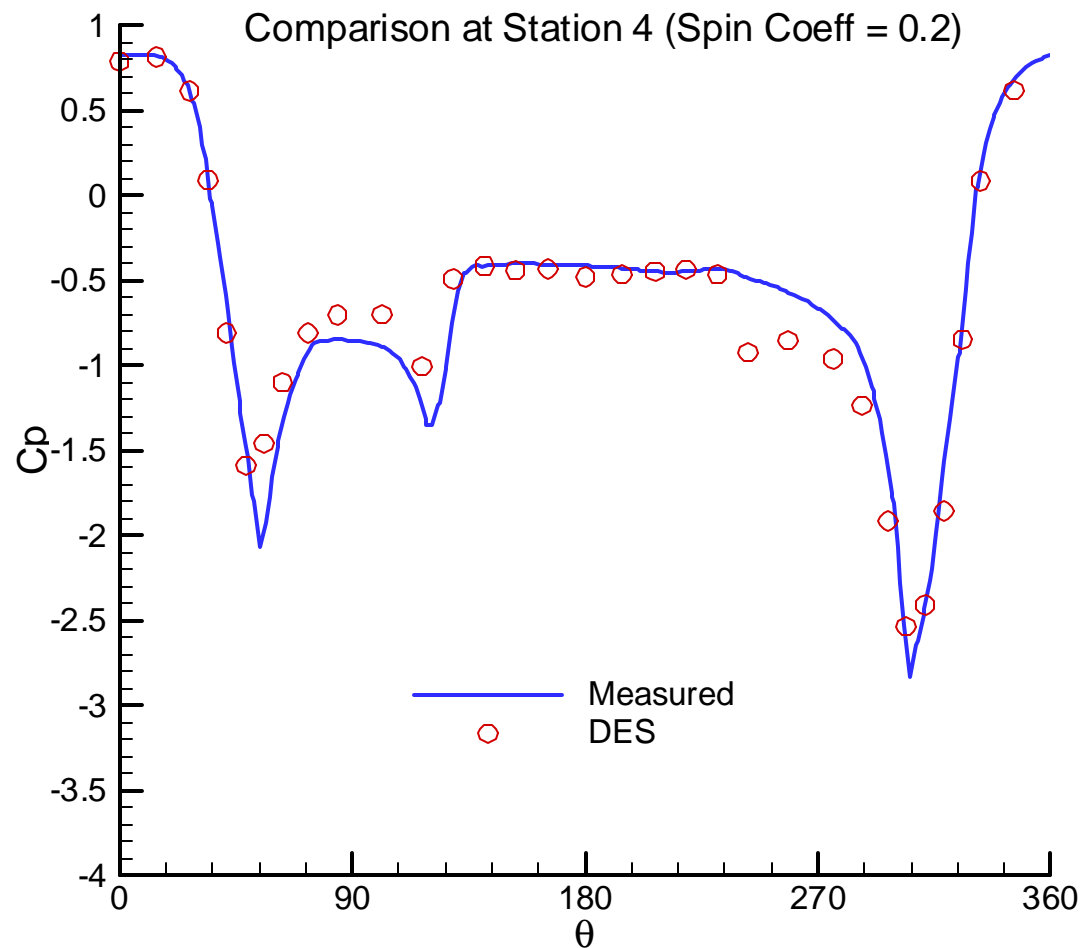


Isosurface of vorticity colored by pressure  
Side and top views



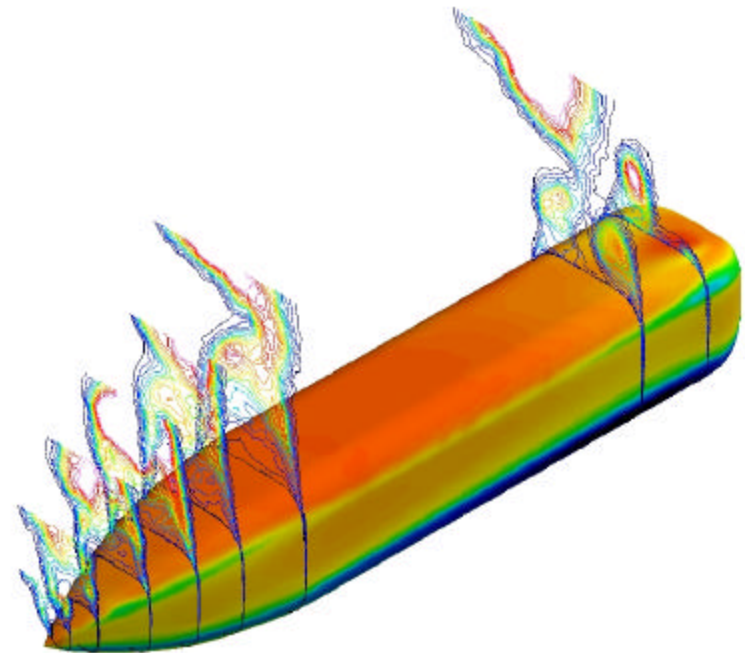
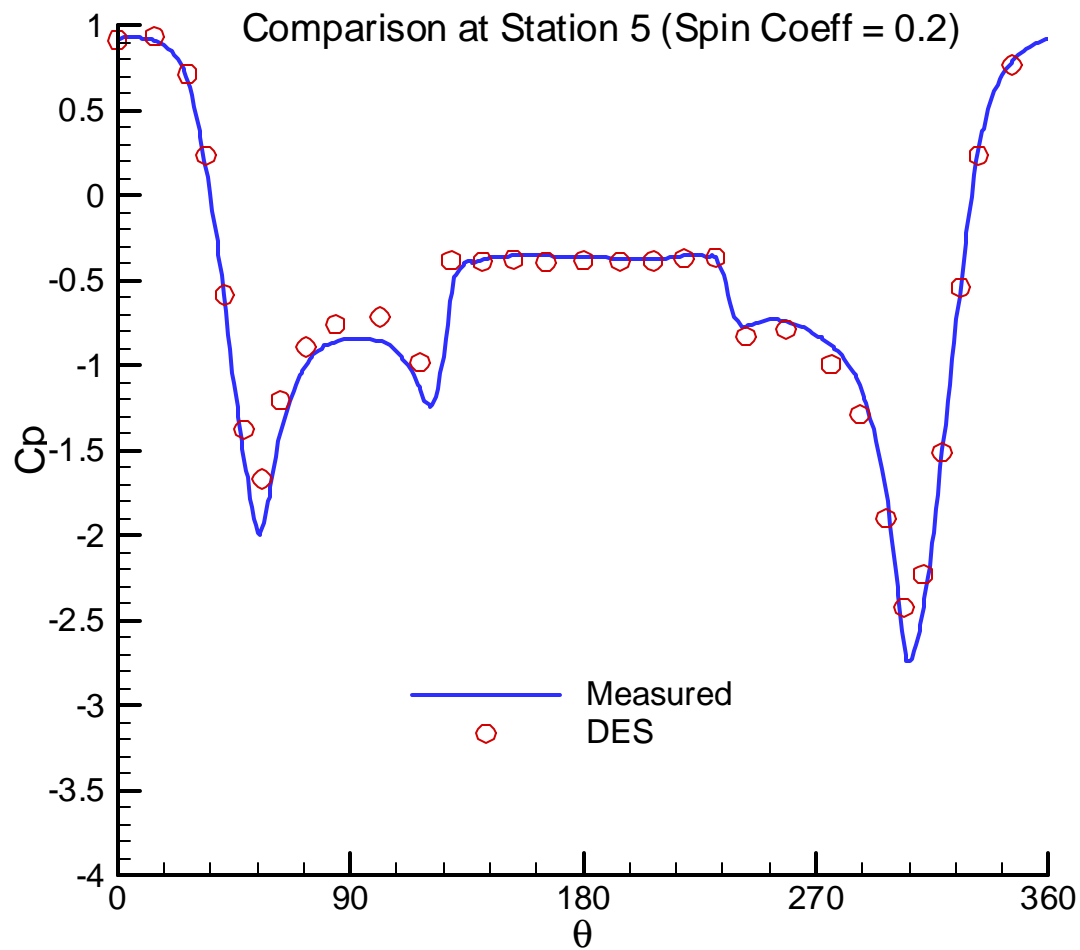


## Azimuthal Pressure Distribution, $Wb/2V = 0.2$





## Azimuthal Pressure Distribution, $Wb/2V = 0.2$





# Preliminary Spin F-15E at 65° angle of attack - DES

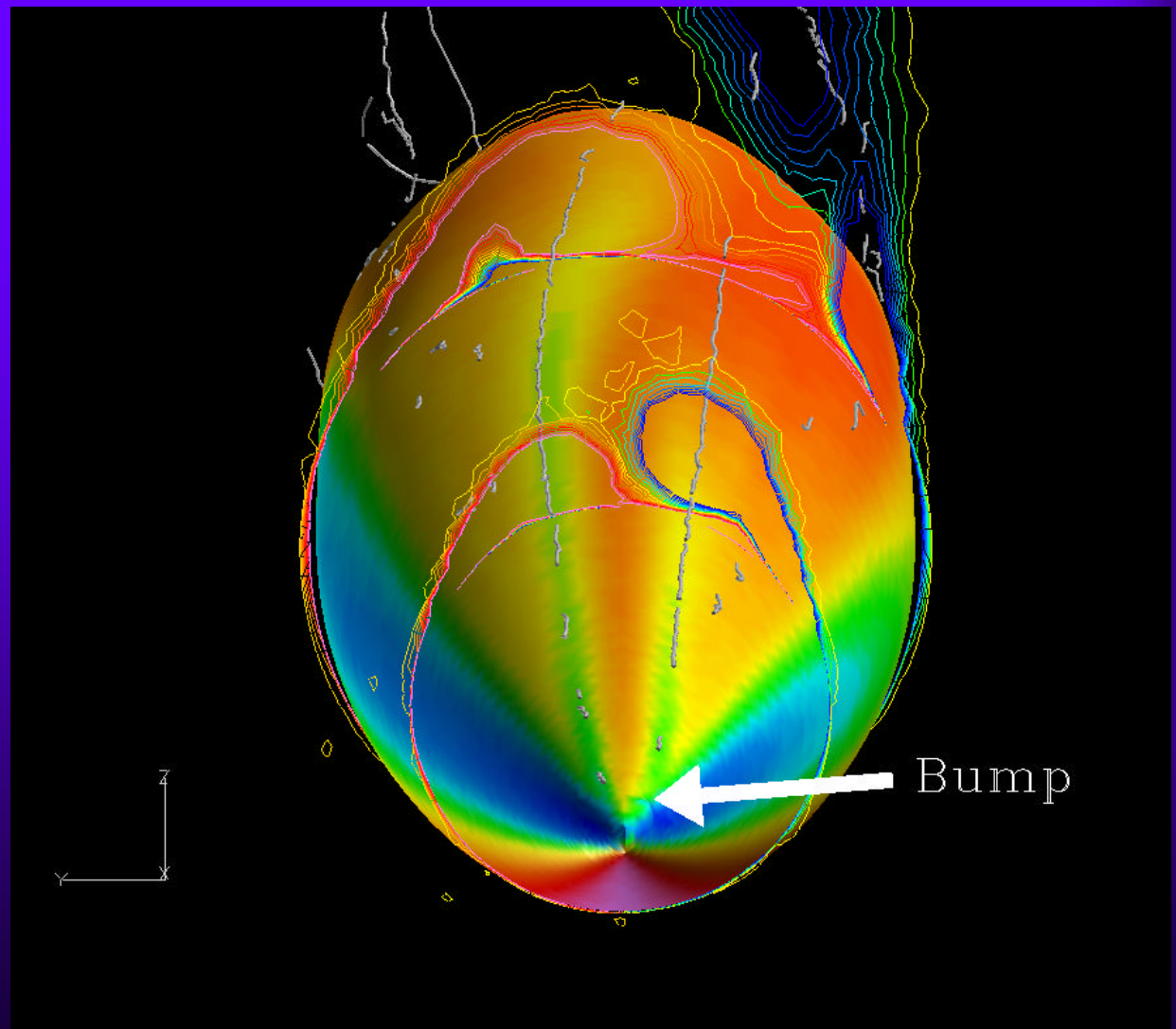


- ♦ grid (full aircraft):  $6.46 \times 10^6$  cells (generated using VGRIDns)
  - prisms in the boundary layers, tetrahedra elsewhere
    - » conversion to prisms using *blacksmith*
  - average first  $y^+ = 0.8$
  - Between resolution of coarse and baseline grids
- ♦ timestep = 0.02 (dimensionless using chord length and freestream speed)
- ♦  $Re = 13.6 \times 10^6$ , Mach number = 0.3
- ♦ rotary motion about centroid along freestream velocity vector



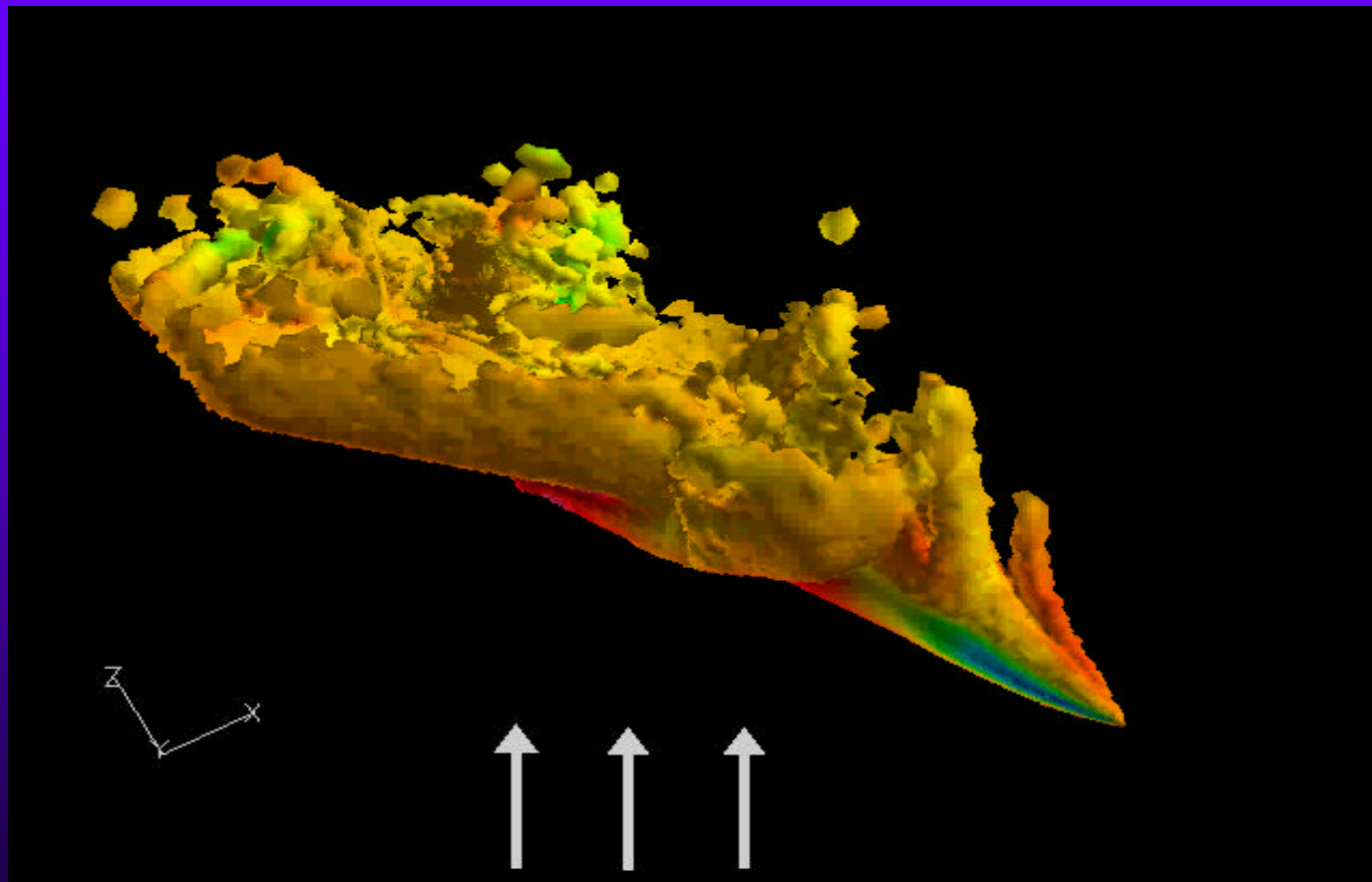
## Asymmetric vortices (zero beta, no spin)

- ▶ Bump added to nose to reproduce strong yawing moment seen in flight test





# Vorticity isosurfaces, colored by pressure Side and top views





# Embedded LES Modifications to Detached Eddy Simulation

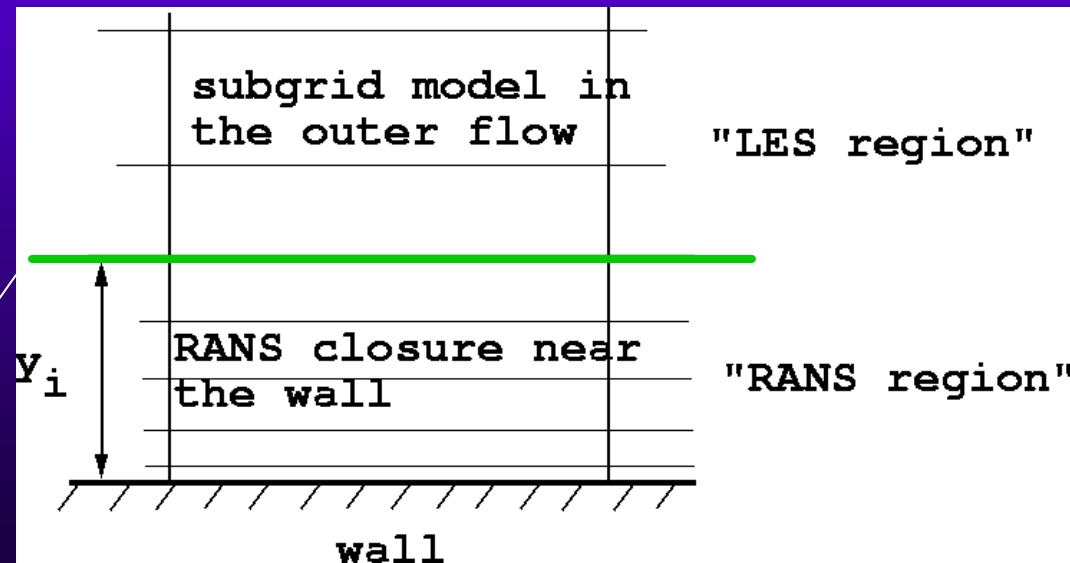




# Research — embedded LES for turbulent channel flow



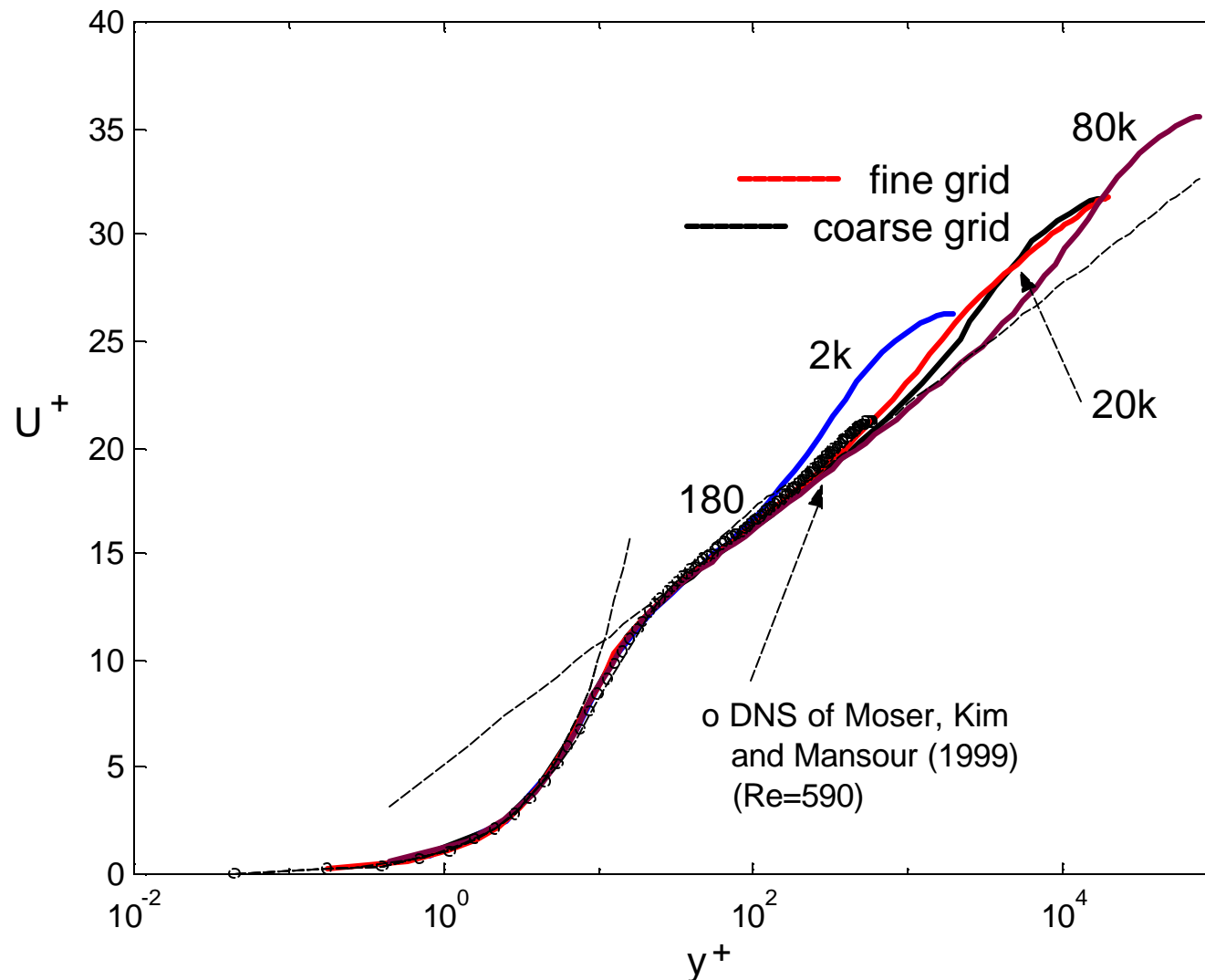
- ♦ importance of including “LES content” in the boundary layer prior to separation
  - flows with shallow separation
  - need grid densities sufficient to sustain eddy content near the wall
- ♦ another view of DES: LES with a complex wall-layer treatment



interface,  $y_i$ , between RANS and LES regions controlled by the grid



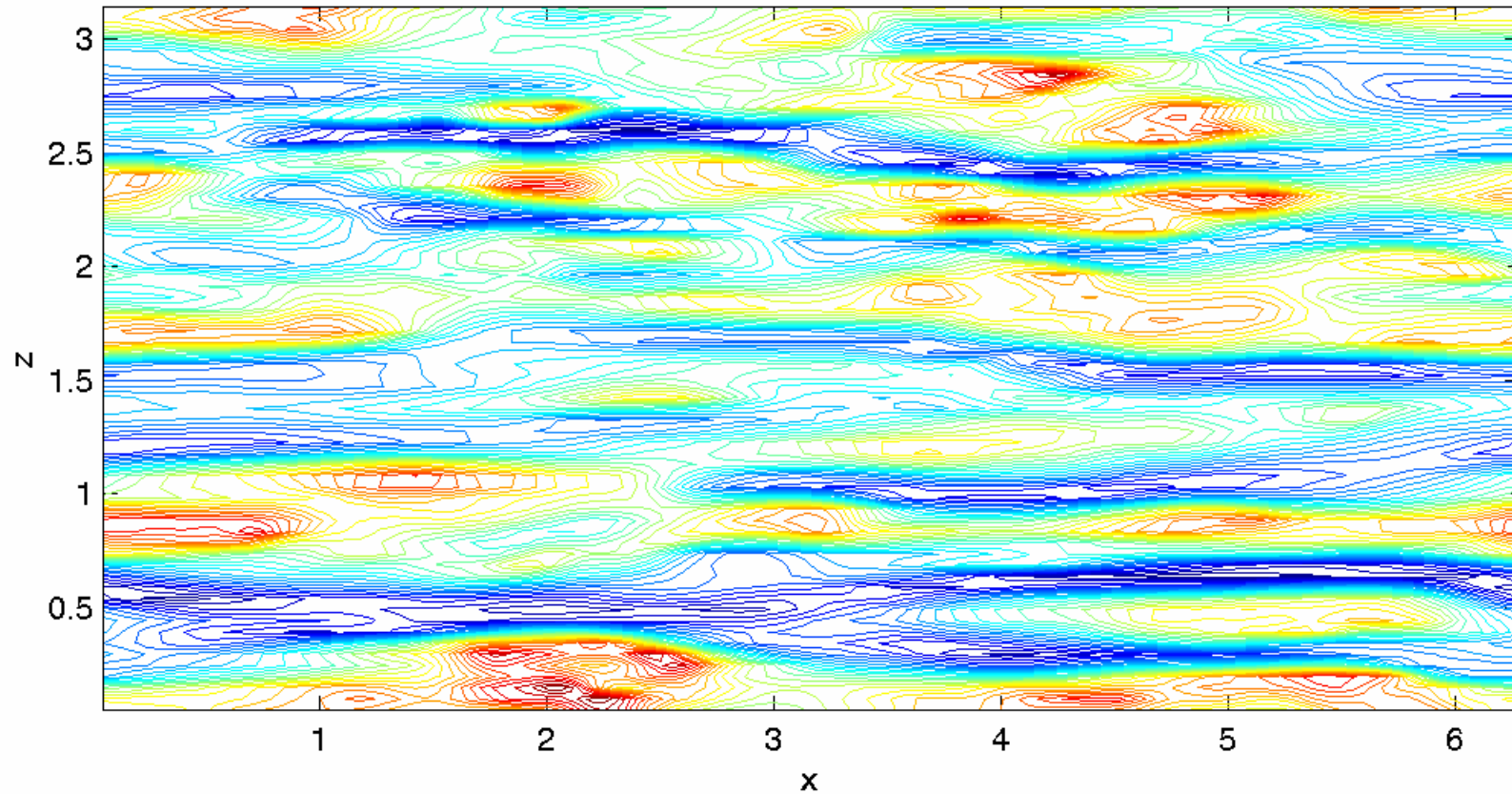
# Mean Velocity



*“super buffer” between RANS and LES velocity profiles  
under-prediction of the skin friction (Nikitin et al. 2000)*

# Flow Structure near RANS-LES interface

u velocity fluctuation, DES, 129x129x65,  $y^+ = 250$



$Re_t = 8000$



# Backscatter



- ♦ **stochastically force the Navier-Stokes equations (Leith 1990, Mason and Thompson 1993, Carati *et al.* 1994...)**

$$\frac{Du_i}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j \partial x_j} - \frac{\partial \tau_{ij}}{\partial x_j} + f_i$$

$f_i$  = stochastic force distributed about RANS-LES interface

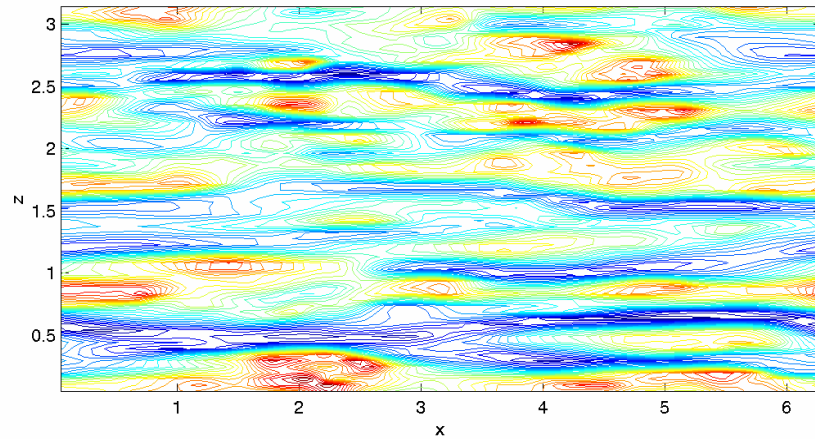
- purely random or scaling using the eddy viscosity, strain rate, and timestep
- ♦ **envelope over which force distributed**

$$e(y; I) = \frac{(I y)^2}{1 + (I y)^4}$$

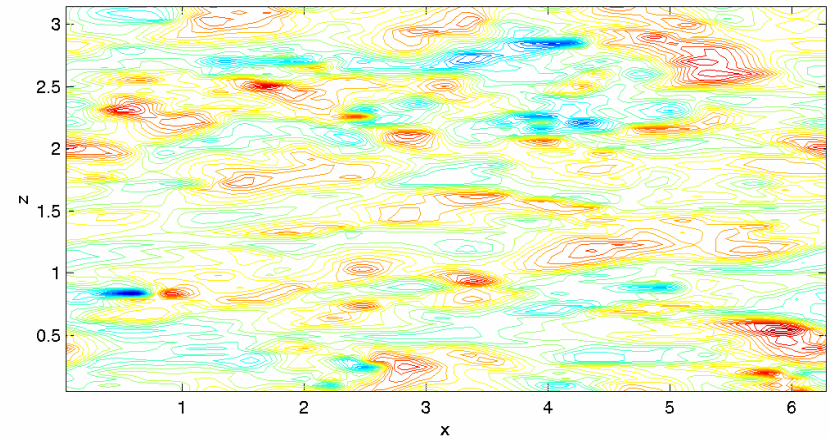
$I$  adjusted so that maximum in envelope at RANS-LES interface

# Flow Structure near RANS-LES interface

u velocity fluctuation, DES, 129x129x65,  $y^+=250$

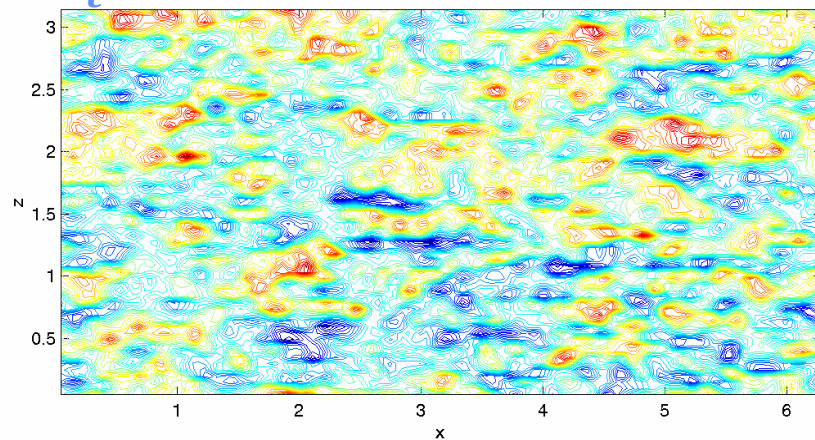


Eddy viscosity, DES, 129x129x65,  $y^+=250$

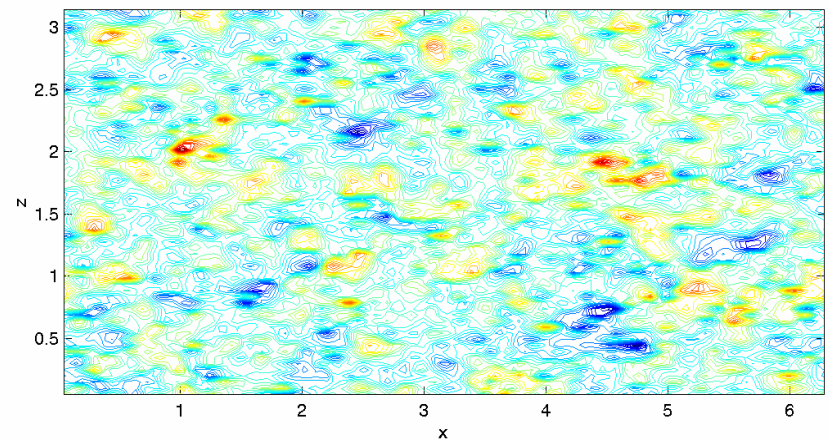


$Re_\tau = 8000$

u velocity fluctuation, DES with backscatter, 129x129x65,  $y^+=250$



Eddy viscosity, DES with backscatter, 129x129x65,  $y^+=250$

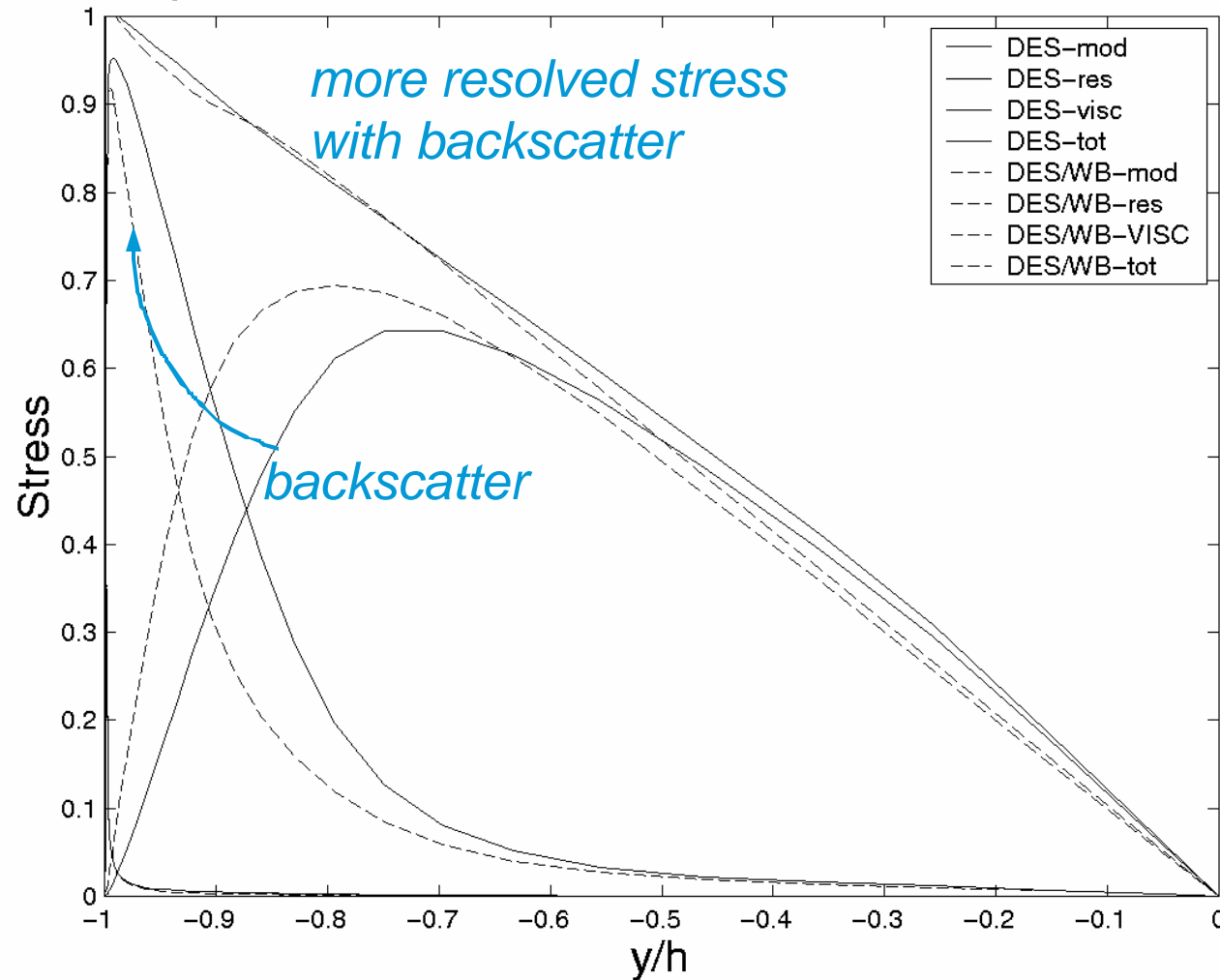




# Turbulent Stresses



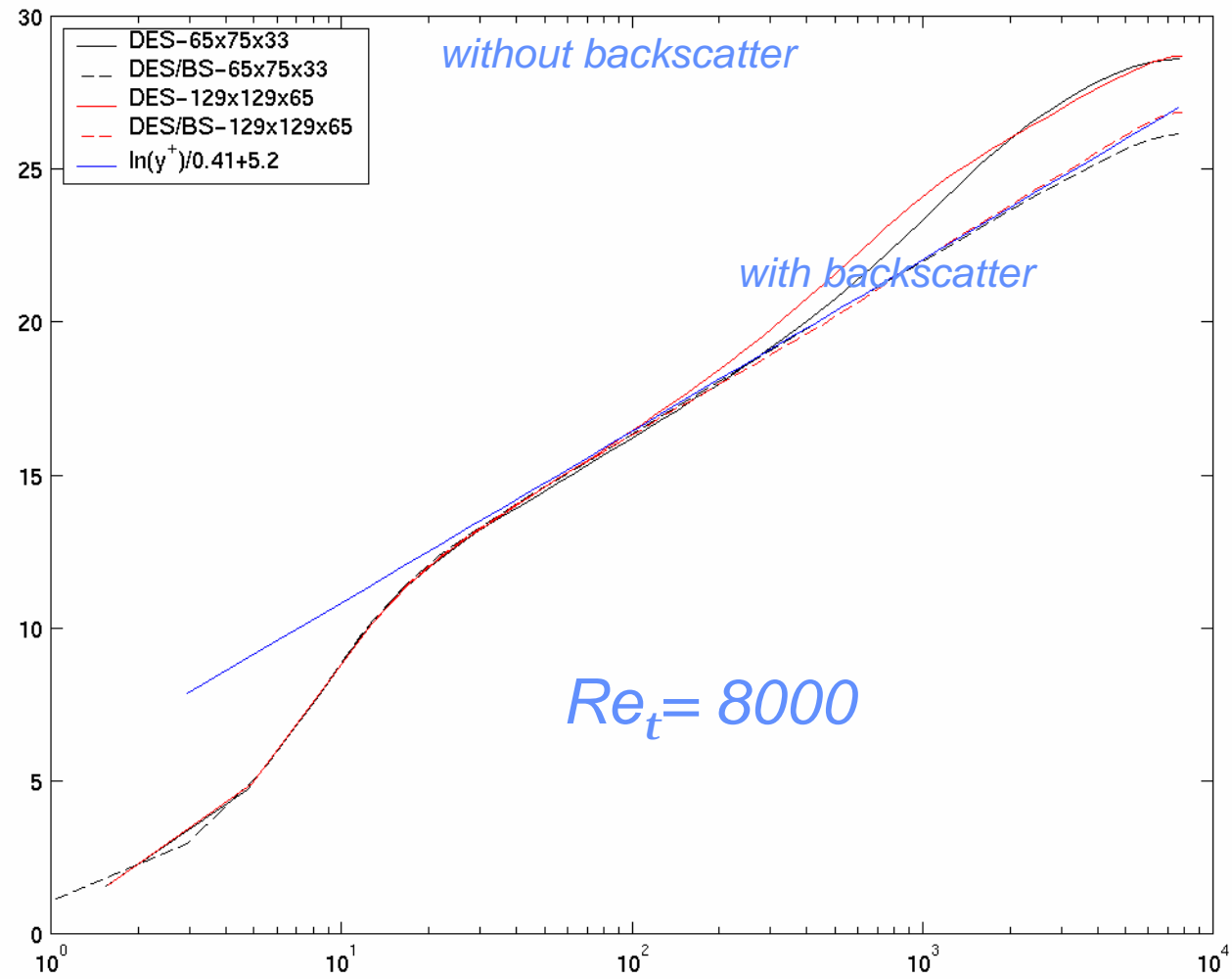
Stress comparison for DES with and without backscatter, 65x75x3



stochastic forcing raises resolved stress, lowers modeled stress



# Mean Velocity





# Future Areas of Research Necessary



- ◆ **Embedded LES to improve simulation of instabilities generated inside the boundary layer**
  - Need to continue the research outlined above
  - Apply the method to more test cases
- ◆ **Unsteady experiments of-**
  - Static high alpha UCAV configurations
  - Pitch and roll maneuver tests with unsteady data gathered
  - Possibly adopt the Boeing 1301 or 1303 as a standard configuration for several groups to test
  - High accuracy methods applied such as PIV, LDV, etc.





# Conclusions



- ◆ **DES has been examined on a wide range of massively separated flows**
  - Moderate to greatly increased accuracy over traditional methods
  - Capability to predict unsteady flows at flight  $Re$ 
    - » Crucial for high alpha maneuvering
    - » Crucial for aero-elasticity, aero-acoustics
  - Enough confidence built to encourage engineering use
- ◆ **Several areas of research needed to apply to super-maneuvering UCAVs with confidence**